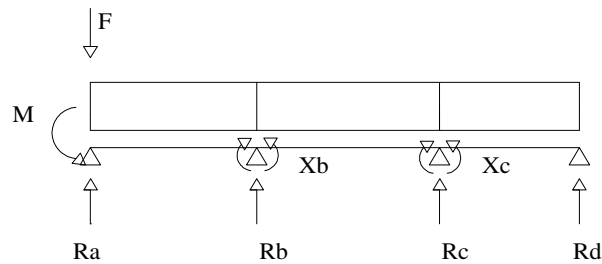
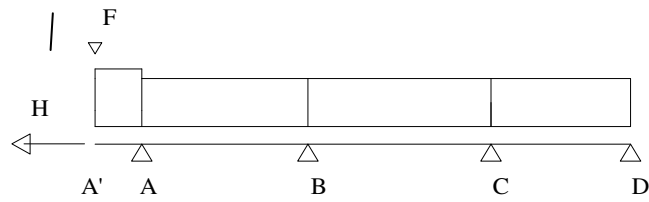


Diagrammi di taglio e momento



Reazioni vincolari

$$R_A = \frac{M}{L_1} + \frac{p_1 L_1}{2} - \frac{X_B}{L_1} + F$$

$$R_B = -\frac{M}{L_1} + \frac{p_1 L_1}{2} + \frac{X_B}{L_1} + \frac{X_B}{L_2} + \frac{p_2 L_2}{2} - \frac{X_C}{L_2}$$

$$R_C = -\frac{X_B}{L_2} + \frac{p_2 L_2}{2} + \frac{X_C}{L_2} + \frac{X_C}{L_3} + \frac{p_3 L_3}{2}$$

$$R_D = -\frac{X_C}{L_3} + \frac{p_3 L_3}{2}$$

Sollecitazione a taglio

$$TA(S) = -F$$

$$TA(D) = TA(S) + RA$$

$$TB(S) = TA(D) - p_2 L_2$$

$$TB(D) = TB(S) + RB$$

$$TC(S) = TB(D) - p_2 L_2$$

$$TC(D) = TC(S) + RC$$

$$TC(D) = TC(D) - p_3 L_3 = -RB$$

Sollecitazioni a momento

$$MA' = -H \times 1,00m$$

$$MA = -M$$

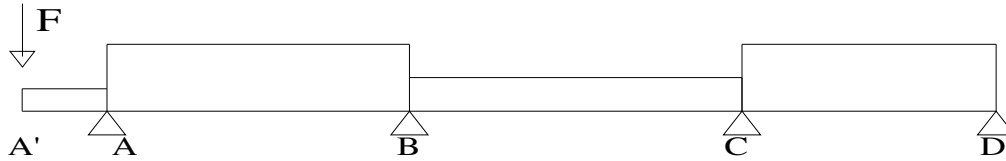
$$MB = -X_B$$

$$MC = -X_C$$

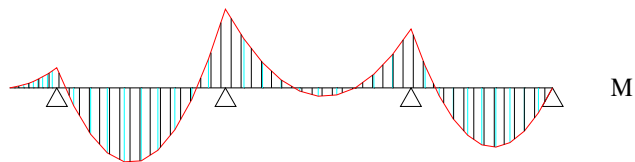
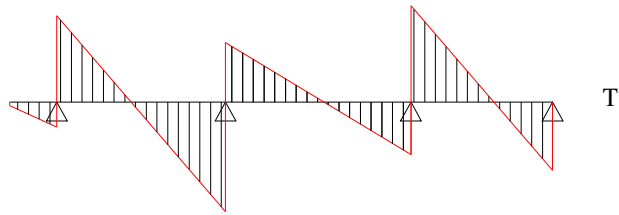
$$MD = 0$$

Combinazione 1 S.L.U.

$q_{d,bc} =$	5.75 kN/m	$M =$	5,66 kN	$L1 =$	5 m
$q_{d,cd} =$	11.05 kN/m	$F_d =$	1,04 kN	$L2 =$	5,5 m
$q_{d,ba} =$	11.05 kN/m	$X_B =$	22,12 kNm	$L3 =$	4,2 m
$q_{d,sb} =$	4.29 kN/m	$X_C =$	16,61 kNm	$L_{sb} =$	1,4 m

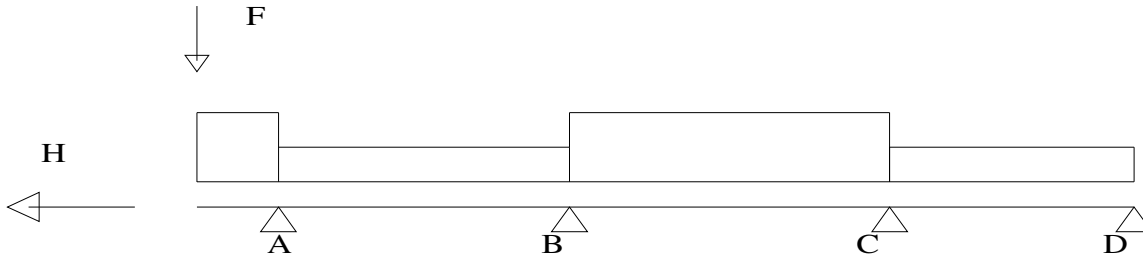


$R_A =$	31.379 kN	$T_A^{(S)} =$	-1,04 kN	$M_{A'} =$	0
$R_B =$	47.7313 kN	$T_A^{(D)} =$	24,33304 kN	$M_A =$	5,6602 kNm
$R_C =$	41.9704 kN	$T_B^{(S)} =$	30,91696 kN	$M_B =$	22,12 kNm
$R_D =$	19.2502 kN	$T_B^{(D)} =$	16,81432 kN	$M_C =$	16,61 kNm
		$T_C^{(S)} =$	14,81608 kN	$M_D =$	0
		$T_C^{(D)} =$	27,15976 kN		
		$T_C^{(D)} =$	19,25024 kN		

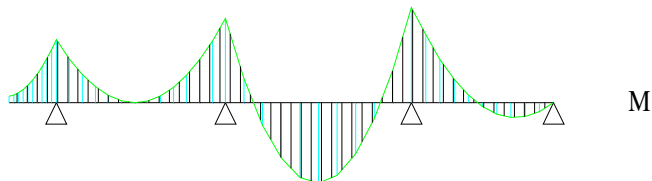
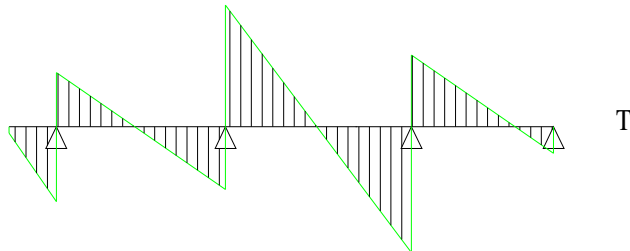


Combinazione 2 S.L.U.

$q_{d,bc} =$	11.05 kN/m	$M = 15,454$ kN	$L1 = 5$ m
$q_{d,cd} =$	5.75 kN/m	$F_d = 1,56$ kN	$L2 = 5,5$ m
$q_{d,ba} =$	5.75 kN/m	$XB = 20,62$ kNm	$L3 = 4,2$ m
$q_{d,sb} =$	12.01 kN/m	$XC = 23,33$ kNm	$L_{sb} = 1,4$ m
		$H_d = 1,5$ kN	

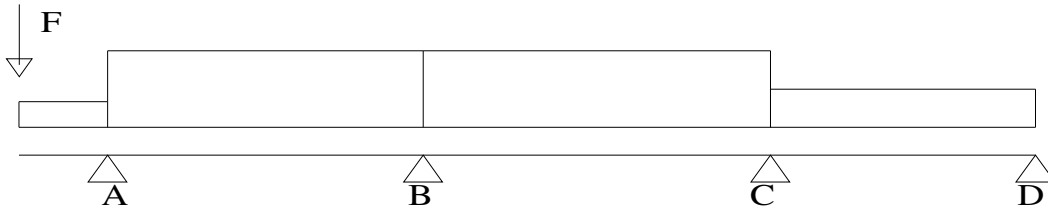


$R_A =$	31.7128 kN	$T_A^{(S)} = -1,56$ kN	$M_A' = -1,5$ kNm
$R_B =$	45.303 kN	$T_A^{(D)} = 13,34176$ kN	$M_A = -15,4538$ kNm
$R_C =$	48.51 kN	$T_B^{(S)} = 15,40824$ kN	$M_B = 20,62$ kNm
$R_D =$	6.52024 kN	$T_B^{(D)} = 29,89477$ kN	$M_C = -23,33$ kNm
		$T_C^{(S)} = 30,88023$ kN	$M_D = 0$
		$T_C^{(D)} = 17,62976$ kN	
		$T_C^{(D)} = 6,520238$ kN	

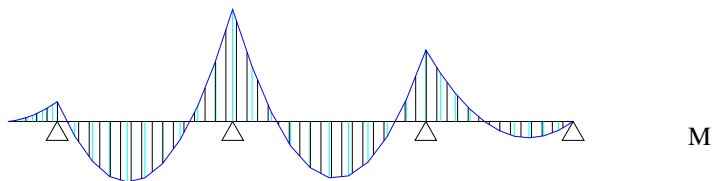
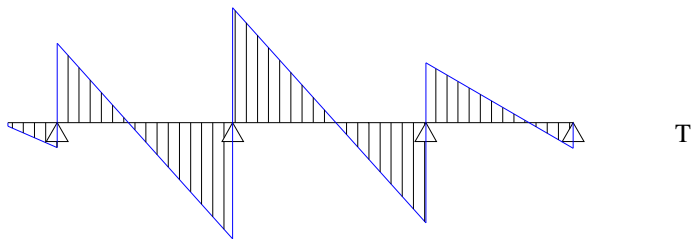


Combinazione 3 S.L.U.

$q_{d,bc} =$	11.05 kN/m	$M =$	5,6602 kN	$L1 =$	5 m
$q_{d,cd} =$	5.75 kN/m	$F_d =$	1,04 kN	$L2 =$	5,5 m
$q_{d,ba} =$	11.05 kN/m	$X_B =$	31,69 kNm	$L3 =$	4,2 m
$q_{d,sb} =$	4.29 kN/m	$X_C =$	20,18 kNm	$L_{sb} =$	1,4 m
		$H_d =$	0 kN		

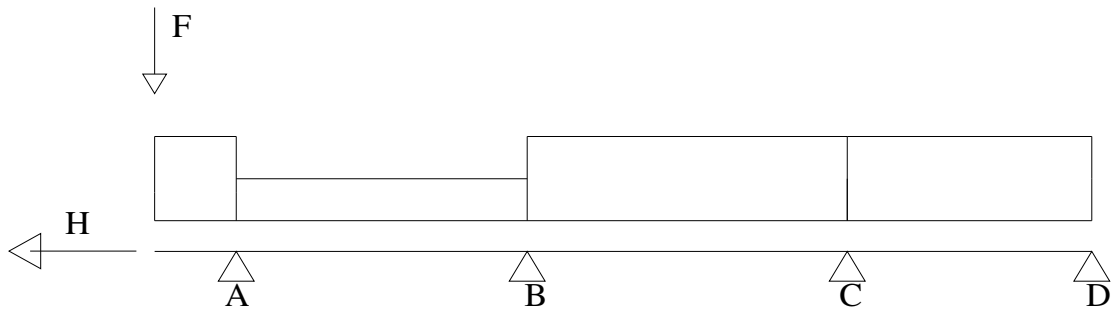


$R_A =$	29.465 kN	$T_A^{(S)} =$	-1,04 kN	$M_A' =$	0 kNm
$R_B =$	65.3112 kN	$T_A^{(D)} =$	22,41904 kN	$M_A =$	-5,6602 kNm
$R_C =$	45.1745 kN	$T_B^{(S)} =$	32,83096 kN	$M_B =$	-31,69 kNm
$R_D =$	7.27024 kN	$T_B^{(D)} =$	32,48023 kN	$M_C =$	-20,18 kNm
		$T_C^{(S)} =$	28,29477 kN	$M_D =$	0
		$T_C^{(D)} =$	16,87976 kN		
		$T_C^{(D)} =$	7,270238 kN		

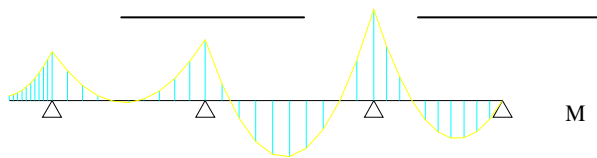
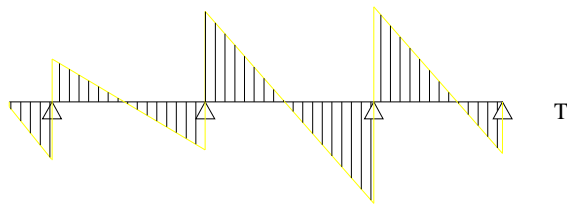


Combinazione 4 S.L.U.

$q_{d,bc} =$	11.05 kN/m	$M = 15,4538$ kN	$L1 = 5$ m
$q_{d,cd} =$	11.05 kN/m	$F_d = 1,56$ kN	$L2 = 5,5$ m
$q_{d,ba} =$	5.75 kN/m	$X_B = 19,23$ kNm	$L3 = 4,2$ m
$q_{d,sb} =$	12.01 kN/m	$X_C = 28,79$ kNm	$L_{sb} = 1,4$ m
		$H_d = 1,5$ kN	

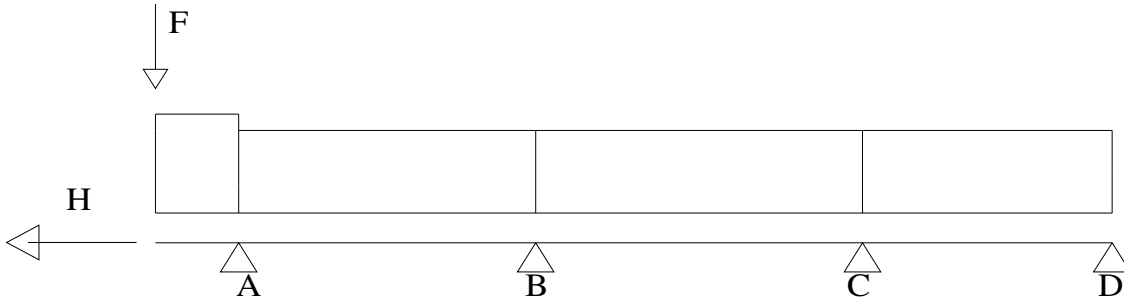


$R_A =$	31.9936 kN	$T_A^{(S)} = -18,374$ kN	$M_A' = -1,5$ kNm
$R_B =$	43.7796 kN	$T_A^{(D)} = 13,61976$ kN	$M_A = -15,4538$ kNm
$R_C =$	62.1854 kN	$T_B^{(S)} = 15,13024$ kN	$M_B = -19,23$ kNm
$R_D =$	16.3602 kN	$T_B^{(D)} = 28,64932$ kN	$M_C = -28,79$ kNm
		$T_C^{(D)} = 32,12568$ kN	$M_D = 0$
		$T_C^{(D)} = 30,05976$ kN	
		$T_C^{(D)} = 16,35024$ kN	

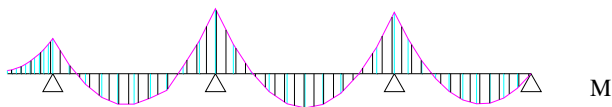
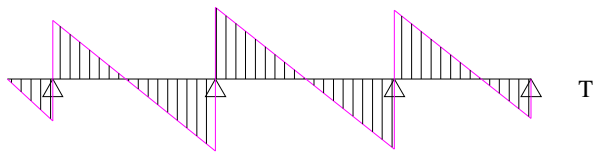


Combinazione 1 S.L.S.

$q_{d,bc} =$	7.75 kN/m	$M =$	10,5802 kN	$L1 =$	5 m
$q_{d,cd} =$	7.75 kN/m	$F_d =$	1,04 kN	$L2 =$	5,5 m
$q_{d,ba} =$	7.75 kN/m	$X_B =$	19,53 kNm	$L3 =$	4,2 m
$q_{d,sb} =$	8.29 kN/m	$X_C =$	18,48 kNm	$L_{sb} =$	1,4 m
		$H_d =$	1 kN		

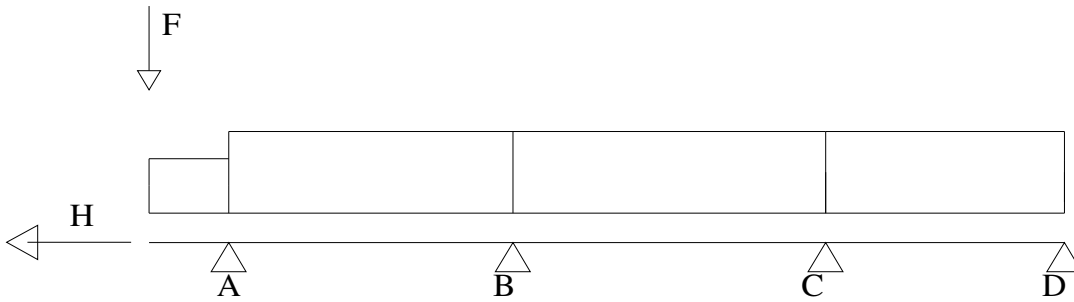


$R_A =$	30.231 kN	$T_A^{(S)} =$	-12,646 kN	$M_A' =$	-1,0 kNm
$R_B =$	42.6684 kN	$T_A^{(D)} =$	17,58504 kN	$M_A =$	-10,5802 kNm
$R_C =$	41.7966 kN	$T_B^{(S)} =$	21,16496 kN	$M_B =$	-19,53 kNm
$R_D =$	11.875 kN	$T_B^{(D)} =$	21,50341 kN	$M_C =$	-18,48 kNm
		$T_C^{(S)} =$	21,12159 kN	$M_D =$	0
		$T_C^{(D)} =$	20,675 kN		
		$T_C^{(D)} =$	11,875 kN		

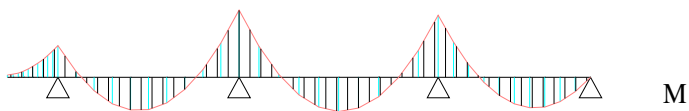
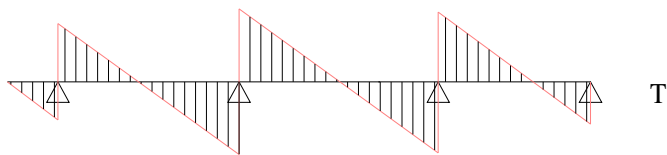


Combinazione 2 S.L.S.

$q_{d,bc} =$	6.75 kN/m	$M =$	8,1202 kN	$L1 =$	5 m
$q_{d,cd} =$	6.75 kN/m	$F_d =$	1,04 kN	$L2 =$	5,5 m
$q_{d,ba} =$	6.75 kN/m	$X_B =$	17,29 kNm	$L3 =$	4,2 m
$q_{d,sb} =$	6.29 kN/m	$X_C =$	15,98 kNm	$L_{sb} =$	1,4 m
		$H_d =$	0,5 kN		

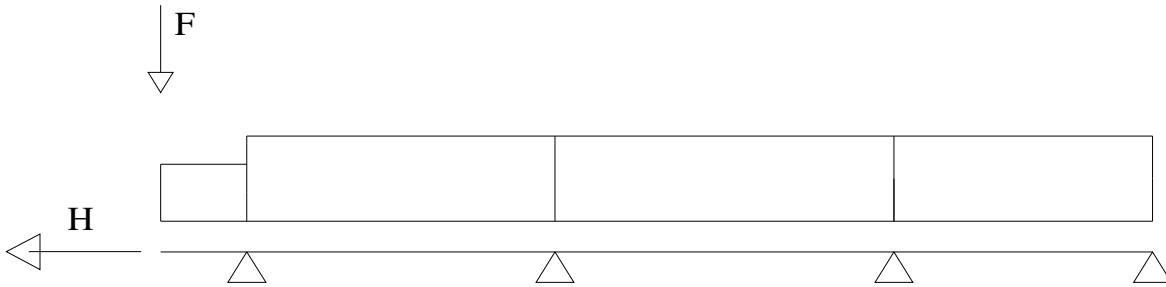


$R_A =$	24.887 kN	$T_A^{(S)} =$	-9,846 kN	$M_A' =$	-0,5 kNm
$R_B =$	37.5096 kN	$T_A^{(D)} =$	15,04104 kN	$M_A =$	-8,1202 kNm
$R_C =$	36.3041 kN	$T_B^{(S)} =$	18,70896 kN	$M_B =$	-17,29 kNm
$R_D =$	10.3702 kN	$T_B^{(D)} =$	18,80068 kN	$M_C =$	-15,98 kNm
		$T_C^{(S)} =$	18,32432 kN	$M_D =$	0
		$T_C^{(D)} =$	17,97976 kN		
		$T_C^{(D)} =$	10,37024 kN		

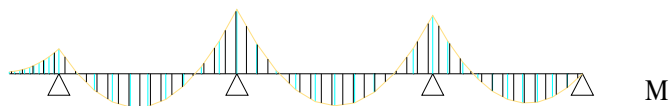
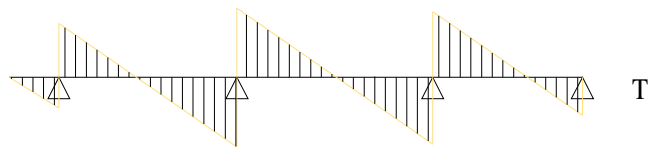


Combinazione 3 S.L.S.

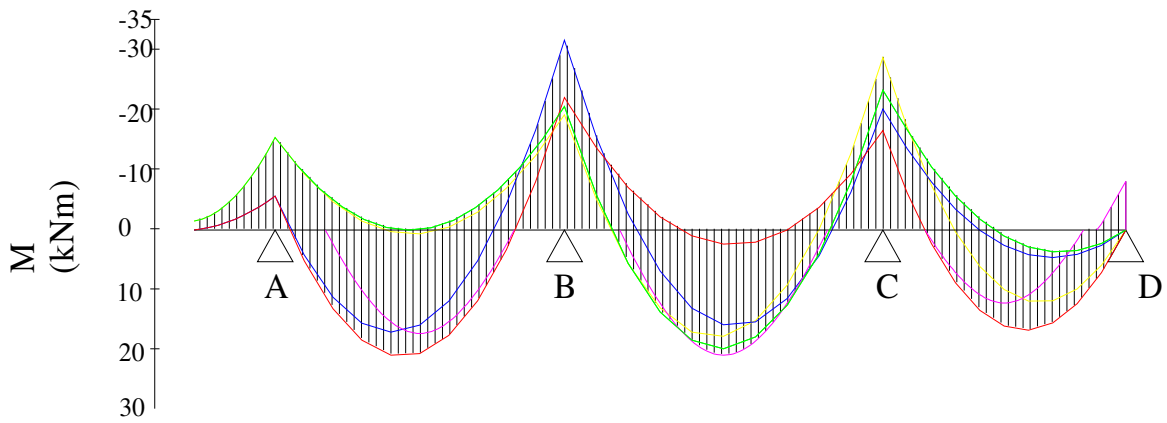
$q_{d,bc} =$	6.15 kN/m	$M =$	6,2162 kN	$L1 =$	5 m
$q_{d,cd} =$	6.15 kN/m	$F_d =$	0,52 kN	$L2 =$	5,5 m
$q_{d,ba} =$	6.15 kN/m	$X_B =$	16,05 kNm	$L3 =$	4,2 m
$q_{d,sb} =$	5.09 kN/m	$X_C =$	14,50 kNm	$L_{sb} =$	1,4 m
		$H_d =$	0,5 kN		



$R_A =$	21.0542 kN	$T_A^{(S)} =$	-7,646 kN	$M_A' =$	-0,5 kNm
$R_B =$	34.5361 kN	$T_A^{(D)} =$	13,40824 kN	$M_A =$	-6,2162 kNm
$R_C =$	32.9981 kN	$T_B^{(S)} =$	17,34176 kN	$M_B =$	-16,05 kNm
$R_D =$	9.46262 kN	$T_B^{(D)} =$	17,19432 kN	$M_C =$	-14,50 kNm
		$T_C^{(S)} =$	16,63068 kN	$M_D =$	0
		$T_C^{(D)} =$	16,36738 kN		
		$T_C^{(D)} =$	9,462619 kN		



Involuppo delle sollecitazioni allo stato limite ultimo



Momenti massimi agli appoggi

$$M_A(\max) = -M_A(4) = -15,4538 \quad \text{kNm}$$

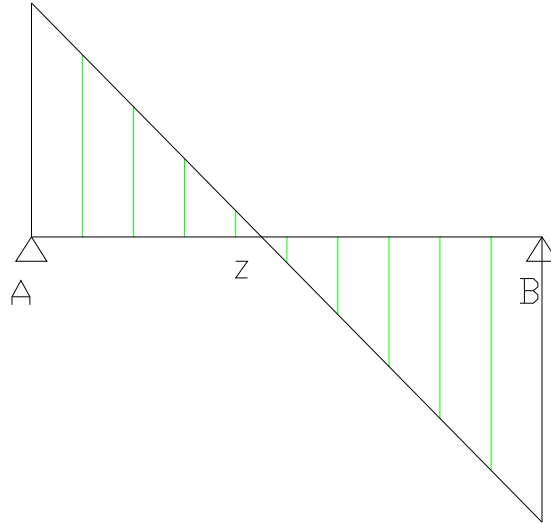
$$M_B(\max) = -X_B(3) = -31,69 \quad \text{kNm}$$

$$M_C(\max) = -X_C(4) = -28,79 \quad \text{kNm}$$

$$M_D(\max) = -\frac{p3L^2}{24} = -8,1 \quad \text{kNm}$$

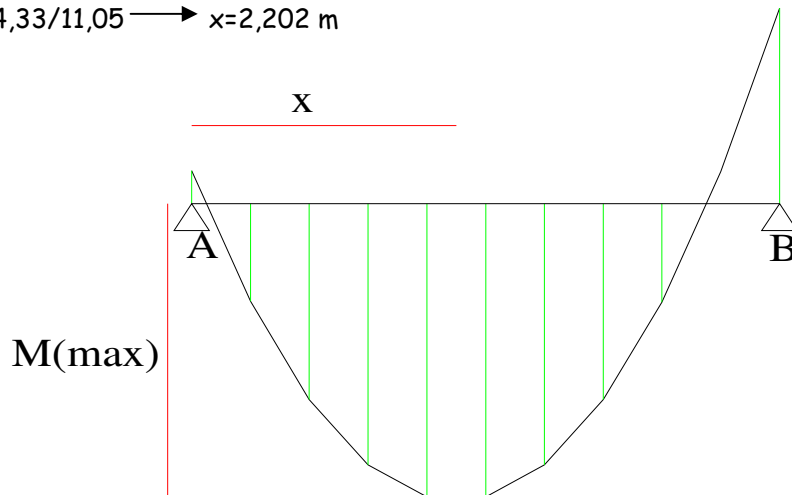
Momenti massimi in campata:

$M_{AB}(\max)$ è data dalla soluzione SLU1 in corrispondenza del punto in cui il taglio è nullo



$$T_A^{(D)} = 24,33 \text{ kN} \quad T_B^{(S)} = -30,91 \text{ kN}$$

$$T_A - qx = 0 \quad q = 11,05 \text{ kN/m}$$
$$24,33 - 11,05x = 0$$
$$x = 24,33 / 11,05 \longrightarrow x = 2,202 \text{ m}$$



$$M_A = -5,66 \text{ kNm}$$

$$M_B = -22,12 \text{ kNm}$$

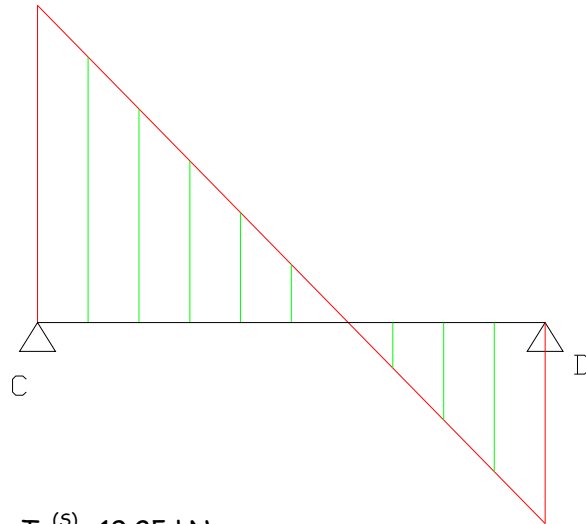
$$M(x) = qx^2/2 + T_A x$$

$$M_{AB}(\max) = 11,05 * 2,202^2 / 2 + 24,33 * 2,202 \quad \longrightarrow \quad 26,785 \text{ kNm}$$

MBC(max) e il momento in campata dovuto al semincastro:

$$MBC(\max) = p(\max)2L^2/16 = 20,89 \text{ KNm}$$

MBC(max) è data dalla soluzione SLU1 in corrispondenza del punto in cui il taglio è nullo

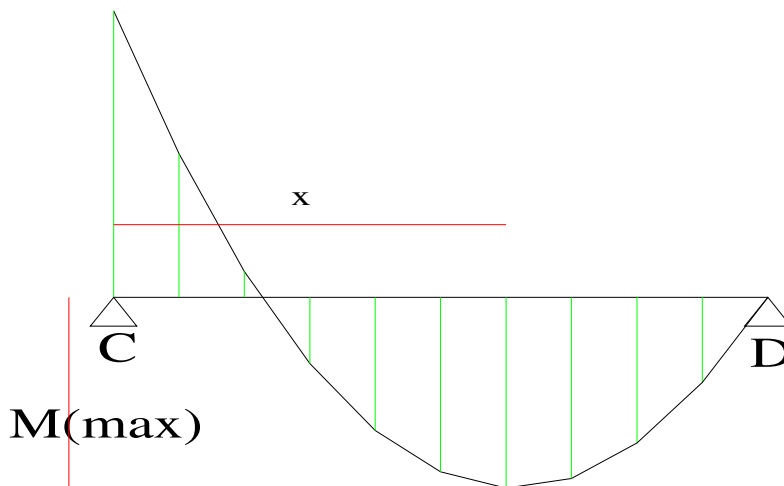


$$T_C^{(D)} = 30,059 \text{ KN} \quad T_D^{(S)} = 19,25 \text{ KN}$$

$$T_A - qx = 0 \quad q = 11,05 \text{ KN/m}$$

$$30,059 - 11,05x = 0$$

$$x = 30,059/11,05 \rightarrow x = 2,72 \text{ m}$$



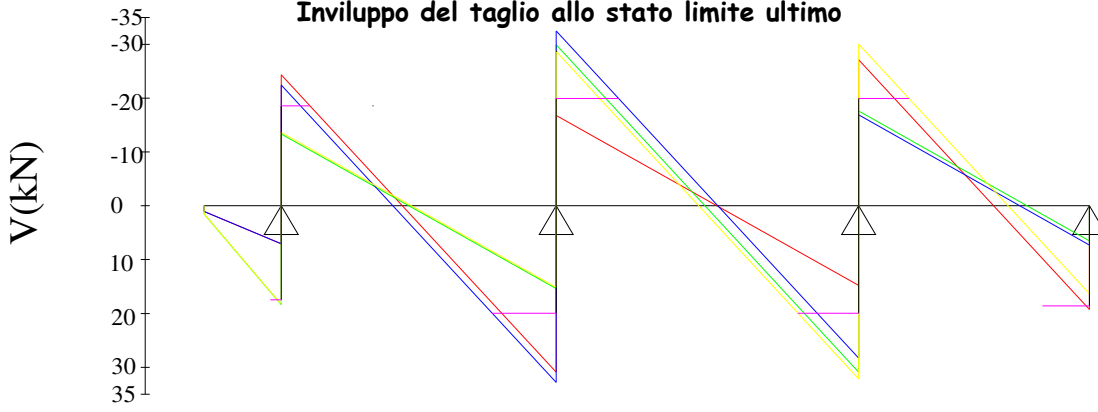
$$M_C = -28,79 \text{ KNm}$$

$$M_B = 0 \text{ KNm}$$

$$M(x) = qx^2/2 + T_Ax$$

$$M_{AB}(\max) = 11,05 \cdot 2,72^2/2 - 30,059 \cdot 2,72 = -40,884 \text{ KNm}$$

Involuppo del taglio allo stato limite ultimo



$$T_A = \begin{cases} T_A^- = -18,374 \text{ KN} \\ T_A^+ = 24,33 \text{ KN} \end{cases}$$

$$T_B = \begin{cases} T_B^- = -32,83 \text{ KN} \\ T_B^+ = 32,48 \text{ KN} \end{cases}$$

$$T_C = \begin{cases} T_C^- = -32,12 \text{ KN} \\ T_C^+ = 30,059 \text{ KN} \end{cases}$$

$$T_D = 19,25 \text{ KN}$$